

Broad categories of fluid flow and canonical geometries

Category

Canonical geometry

Internal Flows

Circular pipe

exact laminar
 D_h turbulent

non-circular ducts

h_m

transitions: contraction or diffuser

fittings

h_p, h_t

pumps/turbines

$$\frac{P_1}{\rho} + z_1 + \alpha_1 \frac{V_1^2}{2g} + h_p = \frac{P_2}{\rho} + z_2 + \alpha_2 \frac{V_2^2}{2g} + h_t + h_e + \sum h_m$$

External Flows

Re Re_{crit}

slender bodies

flat plate 0.66

C_D

bluff body
 appendages

Sphere: Stokes flow

$$\frac{F}{\mu U R} = 6\pi$$

$$C_D = 24/Re$$

$$2/3 C_f \approx 1/3 C_p$$

Free shear flows

mixing layers

2D

jets

2D and axis

wakes

2D and axis

Circular pipe

laminar flow $Re = \frac{U_{max} D}{\nu} < 2000$

$$u(r) = u_{max} \left(1 - \frac{r^2}{R^2}\right) \quad u_{max} = \frac{R^2}{4\mu} \left(-\frac{d\hat{p}}{dx}\right) \quad \hat{p} = p + \rho z$$

$$\tau_w = \frac{8\mu U_{max}}{D}$$

$$\Delta h = h_1 - h_2 = h_L = f \frac{L}{D} \frac{V^2}{2}$$

Re only determines transition; since,

$$f = 64/Re \quad \zeta_f = 16/Re \quad Po = \zeta_f Re = 16$$

creeping flow and no inertia forces and thus absent

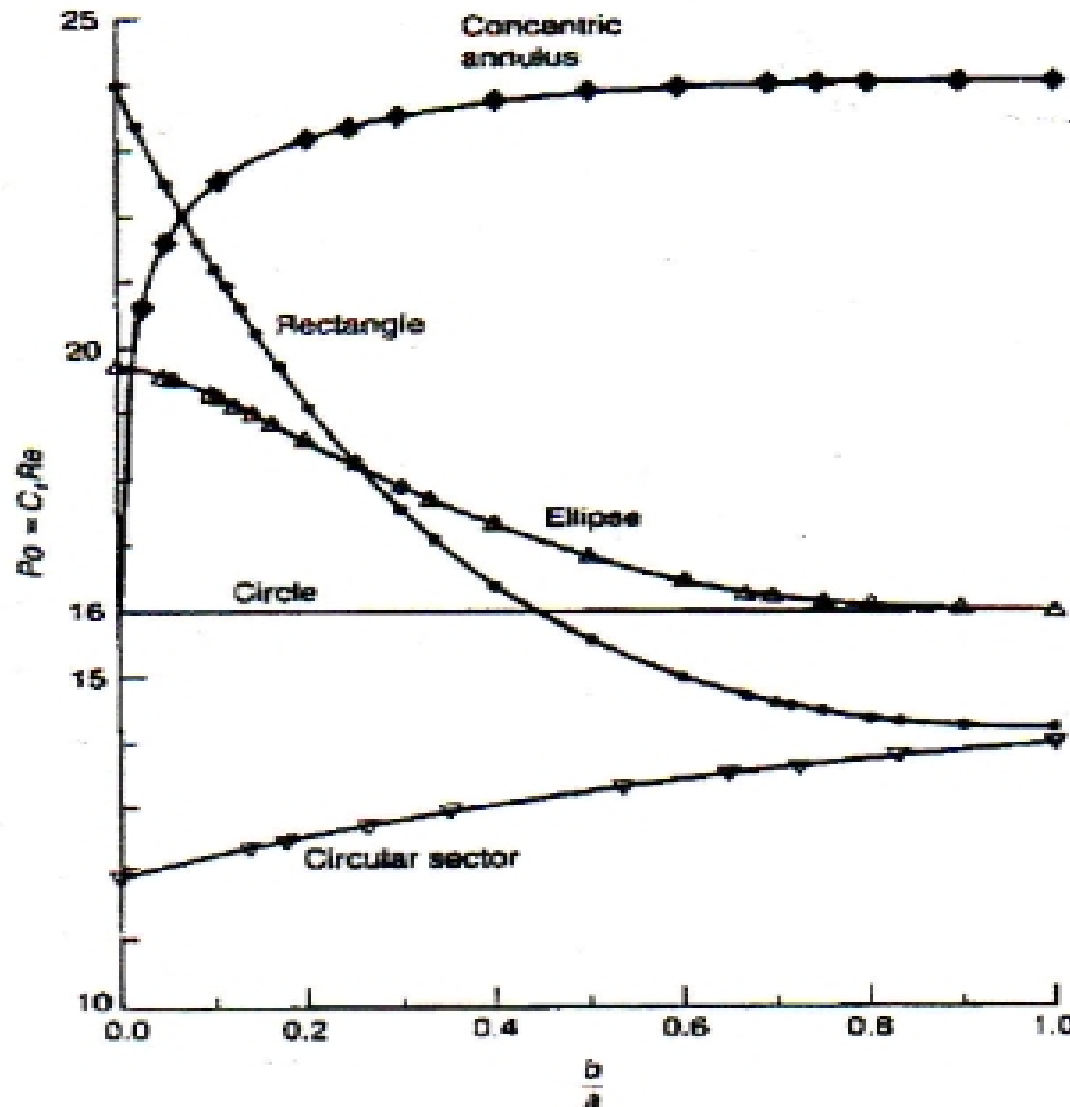


FIGURE 3-13 Comparison of Poiseuille numbers for various duct cross sections when Reynolds number is scaled by the hydraulic diameter. [Numerical data taken from Shah and London (1978).]

turbulent flow

Kolmogorov Scales:

$$\varepsilon = \frac{u_0^3}{L_0} = \frac{u_0^3}{l_0}$$

$u_0^2 = k_2 = \text{kinetic energy}$

$l_0 = L_0 = \text{width of flow}$

is size of largest eddy

dissipation = $\frac{d}{dt} (\text{KE})$ where $\frac{d(\text{KE})}{dt}$ is from largest scales

ε occurs at smallest scales (energy cascade)

at which turbulence is isotropic at low

Reynolds number

$$\eta = (v^3 / \varepsilon)^{1/4}$$

length

$$\eta / l_0 = Re^{-3/4}$$

$$u_\eta = (\varepsilon \eta)^{1/4}$$

velocity

$$u_\eta / u_0 = Re^{-1/4}$$

$$\tau_\eta = (v / \varepsilon)^{1/2}$$

time

$$\tau_\eta / \tau_0 = Re^{-1/2}$$

micro scale \ll large scale at range of
scales where Re power law