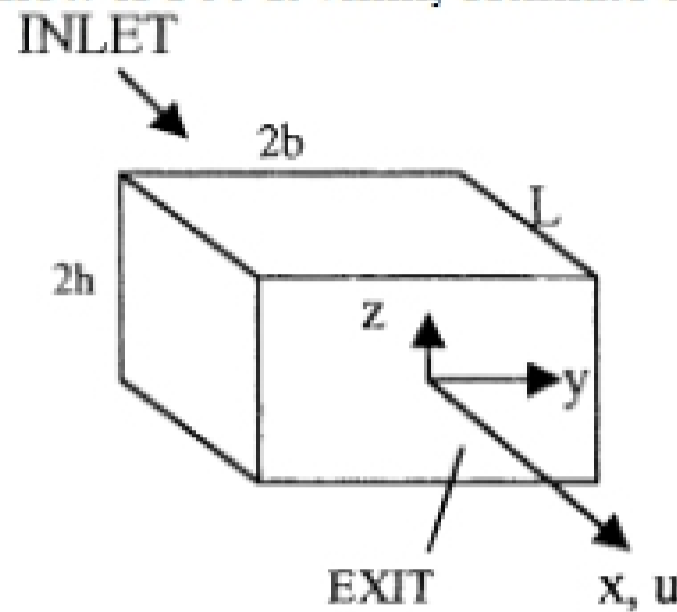


P3.18 An incompressible fluid flows steadily through the rectangular duct in the figure. The exit velocity profile is given by $u \approx u_{\max}(1 - y^2/b^2)(1 - z^2/h^2)$. (a) Does this profile satisfy the correct boundary conditions for viscous fluid flow? (b) Find an analytical expression for the volume flow Q at the exit. (c) If the inlet flow is $300 \text{ ft}^3/\text{min}$, estimate u_{\max} in m/s .



Solution: (a) The fluid should not slip at any of the duct surfaces, which are defined by $y = \pm b$ and $z = \pm h$. From our formula, we see $\mathbf{u} = \mathbf{0}$ at all duct surfaces, OK. *Ans. (a)*

(b) The exit volume flow Q is defined by the integral of u over the exit plane area:

$$Q = \iint u \, dA = \int_{-h}^{+h} \int_{-b}^{+b} u_{\max} \left(1 - \frac{y^2}{b^2}\right) \left(1 - \frac{z^2}{h^2}\right) \, dy \, dz = u_{\max} \int_{-b}^{+b} \left(1 - \frac{y^2}{b^2}\right) \, dy \int_{-h}^{+h} \left(1 - \frac{z^2}{h^2}\right) \, dz = u_{\max} \left(\frac{4b}{3}\right) \left(\frac{4h}{3}\right)$$

$$= \frac{16bhu_{\max}}{9} \quad \text{Ans. (b)}$$

(c) Given $Q = 300 \text{ ft}^3/\text{min} = 0.1416 \text{ m}^3/\text{s}$ and $b = h = 10 \text{ cm}$, the maximum exit velocity is

$$Q = 0.1416 \frac{\text{m}^3}{\text{s}} = \frac{16}{9} (0.1 \text{ m})(0.1 \text{ m}) u_{\max}, \quad \text{solve for } \mathbf{u}_{\max} = 7.96 \text{ m/s} \quad \text{Ans. (c)}$$

P3.33 In some wind tunnels the test section is perforated to suck out fluid and provide a thin viscous boundary layer. The test section wall in Fig. P3.33 contains 1200 holes of 5-mm diameter each per square meter of wall area. The suction velocity through each hole is $V_f = 8 \text{ m/s}$, and the test-section entrance velocity is $V_1 = 35 \text{ m/s}$. Assuming incompressible steady flow of air at 20°C , compute (a) V_0 , (b) V_2 , and (c) V_f , in m/s .

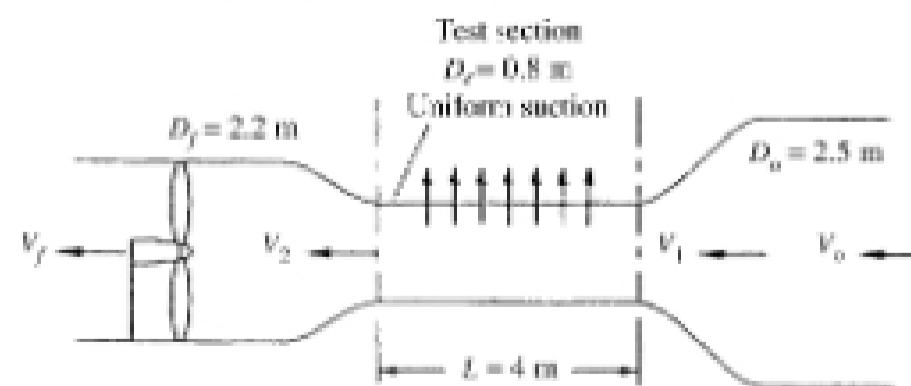


Fig. P3.33

$$\text{Area of test section} = 2\pi rL = 2\pi(0.4m)(4m) = 10.053m^2$$

The number of holes on the test section is $1m^2 : 1200 = 10.0531 : N$, $N = 12064$

$$Q_{\text{suction}} = NQ_{\text{hole}} = NAV_v = (12064)(\pi/4)(0.005 m)^2(8 m/s) \approx 1.895 m^3/s$$

$$(a) \text{ Find } V_o: Q_o = Q_1 \text{ or } V_o \frac{\pi}{4}(2.5)^2 = (35) \frac{\pi}{4}(0.8)^2,$$

$$\text{solve for } V_o \approx 3.58 \frac{m}{s} \text{ Ans. (a)}$$

$$(b) Q_2 = Q_1 - Q_{\text{suction}} = (35) \frac{\pi}{4}(0.8)^2 - 1.895 = V_2 \frac{\pi}{4}(0.8)^2,$$

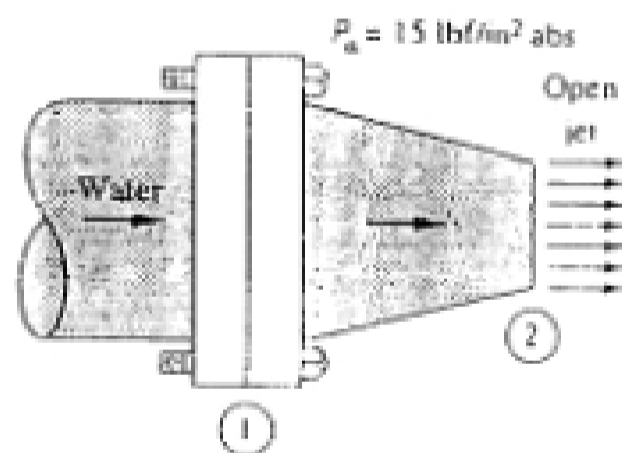
$$\text{or: } V_2 \approx 31.2 \frac{m}{s} \text{ Ans. (b)}$$

$$(c) \text{ Find } V_f: Q_f = Q_2 \text{ or } V_f \frac{\pi}{4}(2.2)^2 = (31.2) \frac{\pi}{4}(0.8)^2,$$

$$\text{solve for } V_f \approx 4.13 \frac{m}{s} \text{ Ans. (c)}$$

P3.49 The horizontal nozzle in Fig. P3.49 has $D_1 = 12$ in, $D_2 = 6$ in, with $p_1 = 38$ psia and $V_2 = 56$ ft/s. For water at 20°C , find the force provided by the flange bolts to hold the nozzle fixed.

Solution: For an open jet, $p_2 = p_a = 15$ psia. Subtract p_a everywhere so the only nonzero pressure is $p_1 = 38 - 15 = 23$ psig.



The mass balance yields the inlet velocity:

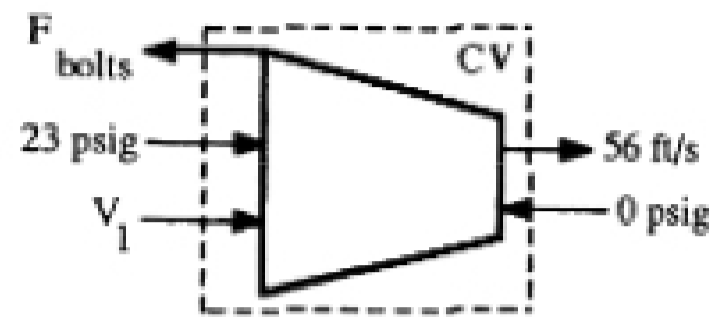
$$V_1 A_1 = V_2 A_2, V_1 \frac{\pi}{4}(12)^2 = (56) \frac{\pi}{4}(6)^2, V_1 = 14 \frac{ft}{s}$$

The density of water is 1.94 slugs per cubic foot. Then the horizontal force balance is

$$\sum F_x = \dot{m}_2 u_2 - \dot{m}_1 u_1$$

$$\sum F_x = -F_{\text{bolts}} + (23 \text{ psig}) \frac{\pi}{4}(12 \text{ in})^2 = \dot{m}_2 u_2 - \dot{m}_1 u_1 = \dot{m}(V_2 - V_1)$$

Compute $F_{\text{bolts}} = 2601 - (1.94) \frac{\pi}{4} (1 \text{ ft})^2 \left(14 \frac{\text{ft}}{\text{s}} \right) \left(56 - 14 \frac{\text{ft}}{\text{s}} \right) \approx 1700 \text{ lbf} \quad \text{Ans.}$



P3.61 A 20°C water jet strikes a vane on a tank with frictionless wheels, as shown. The jet turns and falls into the tank without spilling. If $\theta = 30^\circ$, estimate the horizontal force F needed to hold the tank stationary.

Solution: The CV surrounds the tank and wheels and cuts through the jet, as shown. We should assume that the splashing into the tank does not increase the x -momentum of the water in the tank. Then we can write the CV horizontal force relation:

$$\sum F_x = -F = \frac{d}{dt} \left(\int u \rho dV \right)_{\text{tank}} - \dot{m}_{\text{in}} u_{\text{in}} = 0 - \dot{m} V_{\text{jet}} \quad \text{independent of } \theta$$

$$\text{Thus } F = \rho A_j V_j^2 = \left(1.94 \frac{\text{slug}}{\text{ft}^3} \right) \frac{\pi}{4} \left(\frac{2}{12} \text{ ft} \right)^2 \left(50 \frac{\text{ft}}{\text{s}} \right)^2 \approx 106 \text{ lbf} \quad \text{Ans.}$$

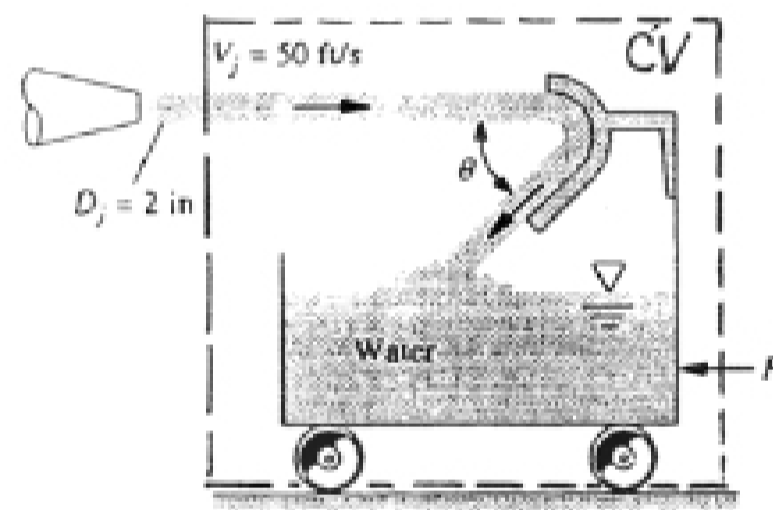


Fig. P3.61